

## DESCRIPTION

## A CONSTANT-VOLTAGE CIRCUIT

5 TECHNICAL FIELD

The present invention generally relates to a constant-voltage circuit, and especially relates to a constant-voltage circuit that is capable of performing phase compensation using a low ESR  
10 (Equivalent Serial Resistance) capacitor by providing a circuit for compensating for a voltage drop of an output voltage caused by an output resistance.

BACKGROUND ART

15 Conventionally, a power unit that is capable of compensating for a voltage drop at a load due to wiring without using two remote sensing lines for low cost has been available, for example, as disclosed by Patent Reference 1.

20 Further, in order to perform phase compensation for a constant-voltage circuit, conventionally, a capacitor is often provided at the output terminal of the constant-voltage circuit in parallel to the load as shown in Fig. 3. An internal  
25 impedance of ESR and a capacitance of a capacitor

C101 provide the phase compensation, and improve the frequency characteristics of the constant-voltage circuit by moving a pole and generating a zero point in the frequency characteristics. Since the  
5 advantage of this method is that the constant-voltage circuit does not have to provide a terminal for phase compensation, the number of terminals of a power supply IC can be small. For such phase compensation method, a tantalum capacitor having a  
10 great ESR is normally used.

As shown in Fig. 4, the typical ESR of a tantalum capacitor having a capacitance of  $2.2 \mu\text{F}$  ranges from  $1 \Omega$  to  $10 \Omega$ , which ESR provides the zero point at a desirable region in the frequency  
15 characteristics of the constant-voltage circuit for phase compensation, and accordingly, satisfactory phase compensation is available. Nevertheless, recently and continuing, ceramic capacitors that are smaller and lighter-weight than tantalum capacitors,  
20 having a large capacitance, are available with a stable supply at low cost. Accordingly, requirements for using the ceramic capacitor as the capacitor for the phase compensation are increasing.

Here, the ESR of the ceramic capacitor is  
25 small, ranging from  $10 \text{ m}\Omega$  to  $30 \text{ m}\Omega$ , which is 100 to

1000 times smaller than the tantalum capacitor as shown in Fig. 5. Accordingly, when the ceramic capacitor is used for phase compensation, the frequency at which a zero point is obtained moves to  
5 a very high frequency, and suitable phase compensation cannot be obtained.

In order to lower the frequency at which the zero point is obtained, a solution may be to insert a resistor in series with the ceramic  
10 capacitor, the resistor being provided outside of a power supply IC (constant voltage IC). However, it is disadvantageous for space and cost reasons. Accordingly, it is preferred that the resistor be provided inside the power supply IC.

15 Fig. 6 and Fig. 7 show examples of a circuit where a resistor is provided in the power supply IC.

The example shown in Fig. 6 includes a terminal PinVout2, which is an IC package terminal, for connecting a ceramic capacitor, a fixed resistor  
20 R103 having a resistance value of about 100 m $\Omega$  for phase compensation provided between a pad ICP2 of the IC chip and the terminal PinVout2, and an output terminal PinVout1 for outputting a voltage. In a  
25 case like this, since the output current  $i_o$  does not

flow through the fixed resistor R103, the output voltage is stably available.

In the case of the example shown in Fig. 7, the resistance value of the fixed resistor R103 for phase compensation ranges from 100 m $\Omega$  to 10  $\Omega$ , the resistor R103 being provided between a pad ICP of the IC chip and the output terminal PinVout of the IC.

While in the case of the example shown in Fig. 7, the number of IC terminals is smaller than the example of Fig. 6, the output current  $i_o$  flows through the fixed resistor R103. When the output current  $i_o$  becomes great, a voltage drop  $V_{drop}$  ( $=i_o \times$  resistance of R103) across the fixed resistor R103 cannot be neglected. In order to compensate for the voltage drop  $V_{drop}$ , a resistor R104 having a fixed resistance value is inserted between a reference voltage source  $V_{ref}$  and the grounding voltage, a load is connected between the output terminal PinVout and the resistor R104, and the same output current  $i_o$  flows through the fixed resistor R104 and the load.

According to this arrangement, if the output current  $i_o$  increases, a voltage drop across the fixed resistor R104 increases, and a voltage of

the non-inverted input terminal of an error  
amplifying circuit AMP into which the reference  
voltage Vref is input rises. For this reason, an  
internal output voltage Vo of the constant-voltage  
5 circuit is raised, and the voltage drop Vdrop due to  
the fixed resistor R103 is compensated for. In order  
to completely remove the influence of the fixed  
resistor R103, relations between resistors R101 and  
R102 for output voltage detection, and the fixed  
10 resistors R103 and R104 are set as  
$$\frac{\text{(resistance of R101)}}{\text{(resistance of R102)}} = \frac{\text{(resistance of R103)}}{\text{(resistance of R104)}}.$$

However, if  $\frac{\text{(resistance of R101)}}{\text{(resistance of R102)}} < \frac{\text{(resistance of R103)}}{\text{(resistance of R104)}}$ , positive feedback starts  
15 occurring, and the output voltage rises. Accordingly,  
the relations are usually made into  
$$\frac{\text{(resistance of R101)}}{\text{(resistance of R102)}} \geq \frac{\text{(resistance of R103)}}{\text{(resistance of R104)}}.$$

20 [ Patent reference 1] JPA 10-257764  
[ Description of the Invention]  
[ Problem(s) to be solved by the Invention]  
As described above, the example shown in  
Fig. 6 has a problem in that an additional IC  
25 terminal is required as compared with the example

shown in Fig. 7, which problem becomes real when an IC has a limit to the number of terminals. As for the example shown in Fig. 7, since the fixed resistor R104 is inserted between the load and the grounding voltage, the low end voltage of the load, which is connected to the resistor R104, is not equal to the ground voltage, which poses a problem when transmitting/receiving a signal to/from a load that is connected to another power supply.

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#### DISCLOSURE OF THE INVENTION

Accordingly, an object of the present invention is to solve the problems and to offer a constant-voltage circuit that is capable of providing a constant voltage that does not cause a problem in transmitting/receiving a signal to/from a load connected to another power supply. In summary, according to the present invention, a current that is proportional to an output current is provided to a part of resistances for output voltage detection, which raises an internal output voltage of the constant-voltage circuit. In this manner, while a voltage drop through a resistance for phase compensation is compensated for, a small capacitor having a small ESR, like a ceramic capacitor, can be

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used for phase compensation. Further, the low side voltage of the load is made to be equal to the grounding voltage.

[Means for Solving the Problem]

5           The constant-voltage circuit of the present invention for converting an input voltage provided to an input terminal of the constant-voltage circuit into a predetermined constant voltage, and for providing the constant voltage to a  
10 load includes:

          a reference voltage generating circuit unit for generating and outputting a predetermined reference voltage;

          an output voltage detecting unit for  
15 detecting the constant voltage, and generating and outputting a voltage that is proportional to the detected voltage;

          an output transistor for outputting a current provided from the input terminal to the load  
20 according to a control signal;

          an error amplifying circuit unit for providing the control signal for controlling operations of the output transistor so that the proportional voltage become equal to the reference  
25 voltage;

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an output current detecting unit for detecting the current output from the output transistor, and generating and outputting the proportional current that is proportional to the  
5 detected current;

a first resistance connected to the output voltage detecting unit;

a proportional current supply circuit unit for supplying the proportional current that is  
10 proportional to the output current from the output current detecting unit to the first resistance;

a second resistance connected between the output transistor and the load; and

a capacitor connected to a junction where  
15 the second resistance and the load are connected, wherein the second resistance and the capacitor constitute a phase compensating circuit unit for carrying out phase compensation of the error amplifying circuit unit.

20 According to the constant-voltage circuit of the present invention, a resistance value of the first resistance is set such that a product of the resistance value and the proportional current provided by the output current detecting unit become  
25 equal to or less than a voltage drop across the



second resistance.

The constant-voltage circuit is arranged such that the output current detecting unit includes a transistor for output current detection for  
5 outputting the current from the input terminal that is in proportion to a value of the current output from the output transistor according to the control signal from the error amplifying circuit unit.

The constant-voltage circuit is arranged  
10 such that the proportional current supply circuit unit includes a current mirror circuit, to which the current output from the transistor for output current detection is provided.

According to an aspect of the present  
15 invention, the proportional current supply circuit unit of the constant-voltage circuit includes a stack type current mirror circuit.

According to an aspect of the present invention, the proportional current supply circuit  
20 unit of the constant-voltage circuit includes two current mirror circuits that are cascoded.

According to an aspect of the present invention, the proportional current supply circuit unit of the constant-voltage circuit includes a  
25 Wilson type current mirror circuit.

According to an aspect of the present invention, the proportional current supply circuit unit includes:

an operation amplifying circuit, wherein  
5 the output of the output transistor is provided to one of input terminals of the operation amplifying circuit, and the output of the transistor for output current detection is provided to another input terminal of the operation amplifying circuit;

10 a current control transistor for controlling the current output from the transistor for output current detection according to an output of the operation amplifying circuit, and for outputting a control current; and

15 a current mirror circuit that inputs the control current output by the current control transistor, and for outputting a current proportional to the control current to the first resistance.

20 According to an aspect of the present invention, the capacitor of the constant-voltage circuit is small, and a ceramic capacitor, for example, is used.

According to an aspect of the present  
25 invention, a resistance value of the second

resistance in the constant-voltage circuit is set between 50 m $\Omega$  and 10  $\Omega$ .

According to an aspect of the present invention, the second resistance of the constant-voltage circuit is formed by wiring resistance.

According to an aspect of the present invention, the reference voltage generating circuit unit, the output voltage detecting unit, the output transistor, the error amplifying circuit unit, the output current detecting unit, the first resistance, and the proportional current supply circuit unit are integrated as an IC.

According to an aspect of the present invention, the reference voltage generating circuit unit, the output voltage detecting unit, the output transistor, the error amplifying circuit unit, the output current detecting unit, the first resistance, the proportional current supply circuit unit, and the second resistance are integrated as an IC.

According to an aspect of the present invention, the first resistance of the constant-voltage circuit may be connected between the output transistor and the output voltage detecting unit.

[ Effect of the Invention ]

As described above, according to the

constant-voltage circuit of the present invention,  
the internal output voltage of the constant-voltage  
circuit is raised by a current proportional to the  
output current to a part of output voltage detection  
5 resistances. In this manner, the voltage drop by the  
resistance prepared for phase compensation is  
compensated for, and a capacitor having a small  
internal resistance like a ceramic capacitor can be  
used for phase compensation. Further, the low side  
10 voltage of the load is made equal to the grounding  
voltage, providing stable signal transfer to and  
from the load.

#### BRIEF DESCRIPTION OF THE DRAWINGS

15 Fig. 1 is an example circuit diagram of a  
constant-voltage circuit according to a first  
embodiment of the present invention.

Fig. 2 is another example circuit diagram  
of the constant-voltage circuit according to the  
20 first embodiment of the present invention.

Fig. 3 is an example circuit diagram of a  
conventional constant-voltage circuit.

Fig. 4 shows an example of an equivalent  
circuit of a tantalum capacitor.

25 Fig. 5 shows an example of an equivalent

circuit of a ceramic capacitor.

Fig. 6 is an example circuit diagram of a conventional constant-voltage circuit.

Fig. 7 is an example circuit diagram of another conventional constant-voltage circuit.

#### BEST MODE FOR CARRYING OUT THE INVENTION

In the following, embodiments of the present invention are described with reference to the accompanying drawings.

##### [ First Embodiment ]

Fig. 1 shows an example of a circuit of a constant-voltage circuit 1 according to the first embodiment of the present invention.

The constant-voltage circuit 1 includes a constant-voltage circuit unit 2 and a phase compensating circuit unit 3. The constant-voltage circuit unit 2 is for generating a predetermined constant voltage from a supply voltage  $V_{dd}$ , and outputs the constant voltage as an internal output voltage  $V_o$ . The phase compensating circuit unit 3 includes a resistor  $R_3$  and a capacitor  $C_1$ , and performs phase compensation to the constant-voltage circuit unit 2.

The constant-voltage circuit unit 2

further includes an error amplifying circuit AMP1, a reference voltage generating circuit 11 for generating and outputting a predetermined reference voltage  $V_{ref}$  that is provided to a non-inverted

5 input terminal of the error amplifying circuit AMP1, an output transistor M1 that is a PMOS transistor for controlling an output current  $i_o$  that is provided to the phase compensating circuit unit 3 according to a signal output from the error

10 amplifying circuit AMP1, and resistors R1, R2, and R4 for detecting the internal output voltage  $V_o$ . Further, the constant-voltage circuit unit 2 includes a transistor M2 that is a PMOS transistor for detecting the output current  $i_o$ , and a current

15 mirror circuit 12. The current mirror circuit 12 includes PMOS transistors M3 and M4, and NMOS transistors M5 and M6.

In addition, the reference voltage generating circuit 11 serves as the reference

20 voltage generating circuit unit, the error amplifying circuit AMP1 serves as an error amplifying circuit unit, and the resistors R1 and R2 serve as an output voltage detecting unit. Further, the transistor M2 serves as an output current

25 detecting unit, the resistor R4 serves as a first

resistance, the current mirror circuit 12 serves as a proportional current supply circuit unit, and the resistor R3 serves as a second resistance.

The inverted input terminal of the error  
5 amplifying circuit AMP1 is connected to a connection point where the resistors R1 and R2 are connected, and the output terminal of the AMP1 is connected to the gate of the output transistor M1. The output transistor M1 is connected between the supply  
10 voltage Vdd, which is an input voltage, and an output pad 15, called an IC pad 15, of the IC, the IC pad 15 being the output terminal of the constant-voltage circuit unit 2. The resistors R4, R1, and R2 are connected in series between the drain of the  
15 output transistor M1, and the grounding voltage. The gate of the output transistor M1 is connected to the output terminal of the error amplifying circuit AMP1. As for the transistor M2 for output current detection, the source is connected to the supply  
20 voltage Vdd.

Between the drain of the transistor M2 for output current detection, and the grounding voltage, the PMOS transistor M4 and the NMOS transistor M6 are connected in series, and the PMOS transistor M3  
25 and the NMOS transistor M5 are connected in series

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between the connection point of the resistors R4 and R1, and the grounding voltage. The gate of the PMOS transistor M3 and the gate of the PMOS transistor M4 are connected, and the connection point thereof is  
5 connected to the drain of the PMOS transistor M3. Further, the gate of the NMOS transistor M5 and the gate of the NMOS transistor M6 are connected, and the connection point thereof is connected to the drain of the NMOS transistor M6.

10 In the configuration as described above, the error amplifying circuit AMP1 controls the gate voltage of the output transistor M1 so that the voltages of the input terminals of the error amplifying circuit AMP1 become equal to each other.  
15 Accordingly, the internal output voltage  $V_o$  of the constant-voltage circuit unit 2 when the output current  $i_o$  is zero is expressed by the following formula (1). Here in the formula (1), R1, R2, and R4 represent resistance values of the resistors R1, R2,  
20 and R4, respectively.

$$V_o = V_{ref} \times (R_4 + R_1 + R_2) / R_2 \dots\dots\dots (1)$$

The internal output voltage  $V_o$  is provided from the output terminal Pout of the IC through the IC pad 15 and the fixed resistor R3 for phase  
25 compensation. Between the output terminal Pout of



the IC and the grounding voltage, a load 10 is connected with a capacitor C1 for phase compensation in parallel.

Since the fixed resistor R3 for phase  
5 compensation is provided in the IC, a ceramic capacitor having a small ESR can serve as the capacitor C1.

However, as the output current  $i_o$  increases, a voltage drop  $V_{drop}$  increases across the  
10 fixed resistor R3 for phase compensation, and the voltage  $V_{out}$  of the output terminal Pout is decreased accordingly. The transistor M2 for output current detection, the current mirror circuit 12, and the resistor R4 constitute a circuit for  
15 compensating for the voltage drop  $V_{drop}$ .

The gates of the transistor M2 and the transistor M1 are connected, and the sources of the transistor M2 and the transistor M1 are connected, constituting a current mirror circuit. The drain  
20 current of the transistor M2 is set at, e.g., between  $1/10000$  and  $1/1000$  of the drain current of the transistor M1.

The drain current of the transistor M2 is provided to the current mirror circuit 12, the  
25 channel length modulation effect of which is

improved. Although the current mirror circuit 12 shown in Fig. 1 is constituted by a stack type circuit, a cascading current supply, a Wilson type current mirror circuit, and the like may be used.

5           An output current  $i_3$  of the current mirror circuit 12 is taken out as the source current of the PMOS transistor M3. If the mirror current ratio of the current mirror circuit 12 is set at 1:1, the source current  $i_3$  of the PMOS transistor M3 becomes  
10   equal to the drain current of the transistor M2 for output current detection. (Note: Output current  $i_3$  is output as viewed from transistor M1, but input as viewed by transistor M3. This is okay as translated.)

15           Since the source of the PMOS transistor M3 is connected to the connection point of the resistor R4 and the resistor R1, the source current  $i_3$  of the PMOS transistor M3 flows through the resistor R4, and a voltage drop equal to the resistance of R4 x  
20    $i_3$  is generated across the resistor R4. (Note: You are correct that  $i_2 = i_3 + i_1$ , but  $i_3$  is the part that is changing. The translation is good)

          Consequently, since the voltage drop across the resistor R4 increases as the output  
25   current  $i_o$  increases, the internal output voltage  $V_o$

of the constant-voltage circuit unit 2 is raised,  
and the voltage drop  $V_{drop}$  generated by the resistor  
 $R_3$  for phase compensation can be compensated for.

This situation is further explained using  
5 the following formulas. Here, in each formula,  $R_1$   
through  $R_4$  represent resistance values of the  
resistors  $R_1$  through  $R_4$ , respectively.

The internal output voltage  $V_o$  of the  
constant-voltage circuit unit 2 is expressed by the  
10 following formula (2).

$$V_o = V_{ref} \times (R_4 + R_1 + R_2) / R_2 + R_4 \times i_3 \dots (2)$$

Further, the voltage  $V_{out}$  of the output  
terminal  $P_{out}$  is expressed by the following formula  
(3).

15 
$$V_{out} = V_o - R_3 \times i_o \dots \dots \dots (3)$$

By substituting the formula (2) into the  
formula (3), the following formula (4) is obtained.

$$V_{out} = V_{ref} \times (R_4 + R_1 + R_2) / R_2 + R_4 \times i_3 \\ - R_3 \times i_o \dots \dots \dots (4)$$

20 In reference to the formula (4), a  
condition that makes  $R_4 \times i_3 - R_3 \times i_o = 0$  provides an  
ideal voltage compensation.

Accordingly, the condition is  $R_4 \times i_3 = R_3 \times i_o$ .

Provided that  $i_o / i_3 = A$  ( $A$  is a constant),  
25 the condition is that  $R_4 = A \times R_3$ . That is, the

condition is that the resistance of the resistor R4 be A times of the resistance of the resistor R3. However, if  $R4 \times i3$  becomes greater than  $R3 \times i_o$ , positive feedback starts. Accordingly, the value of the constant A is usually set equal to or smaller than  $i_o/i3$ .

Fig. 2 shows another example circuit of a constant-voltage circuit 1a according to the first embodiment of the present invention. Here in Fig. 2, the components the same as in Fig. 1 are given the same reference marks, and explanations thereof are not repeated, but differences are described in the following.

The differences include that the current mirror circuit 12 of Fig. 1 is replaced by a current mirror circuit 12a. The PMOS transistor M3 of the current mirror circuit 12 is not used in the current mirror circuit 12a, wherein an operation amplifying circuit AMP2 is added, and the transistors M5 and M6 constitute a single-stage current mirror circuit. In this connection, the constant-voltage circuit unit is referred to as the constant-voltage circuit unit 2a, and the constant-voltage circuit is referred to as the constant-voltage circuit 1a in Fig. 2.

With reference to Fig. 2, the constant-

voltage circuit 1a includes the constant-voltage circuit unit 2a and the phase compensating circuit unit 3. The constant-voltage circuit unit 2a is for generating a predetermined constant voltage from the supply voltage Vdd, which is an input voltage, and outputs the constant voltage as the internal output voltage Vo. The phase compensating circuit unit 3 performs phase compensation for the internal output voltage Vo output from the constant-voltage circuit unit 2a, and supplies the phase-compensated voltage to the load 10.

The constant-voltage circuit unit 2a includes the reference voltage generating circuit 11, the error amplifying circuit AMP1, the output transistor M1, the resistors R1, R2, and R4 for output voltage detection, the transistor M2 for output current detection, and the current mirror circuit 12a. The current mirror circuit 12a includes the operation amplifying circuit AMP2, the PMOS transistor M4, and the NMOS transistors M5 and M6. In addition, current mirror circuit 12a serves as the proportional current supply circuit unit, and the PMOS transistor M4 serves as a current control transistor.

Between the drain of the transistor M2 for

output current detection, and the grounding voltage, the PMOS transistor M4 and the NMOS transistor M6 are connected in series, and the NMOS transistor M5 is connected between the connection point of the resistors R4 and R1, and the grounding voltage. The gate of the PMOS transistor M4 is connected to the output terminal of the operation amplifying circuit AMP2, the internal output voltage  $V_o$  is provided to the non-inverted input terminal of the operation amplifying circuit AMP2, and the source of the PMOS transistor M4 is connected to the inverted input terminal of the operation amplifying circuit AMP2. Further, the gate of the NMOS transistor M5 and the gate of the NMOS transistor M6 are connected, and the connection point is connected to the drain of the NMOS transistor M6.

In a such configuration, the drain current of the PMOS transistor M4 serves as the input current for the current mirror circuit constituted by the NMOS transistors M5 and M6, and the current mirror circuit provides the drain current of the NMOS transistor M5 to the resistor R4. (Note: Yes, the wording is strange but the arrow is correct.)

In this way, the current mirror circuit constituted by the NMOS transistors M5 and M6 is

inserted in the feedback loop of the operation  
amplifying circuit AMP2. Accordingly, the current  
mirror circuit 12a controls the gate voltage of the  
PMOS transistor M4 so that the drain voltage of the  
5 output transistor M1 and the drain voltage of the  
transistor M2 for output current detection are made  
equal. For this reason, precision of the current of  
the current mirror circuit 12 can be further raised  
as compared with the case shown by Fig. 1.

10 As described above, the constant-voltage  
circuit according to the first embodiment of the  
present invention is capable of compensating for not  
only the voltage drop across the resistor R3 for  
phase compensation connected to the IC pad 15, but  
15 also a gain fall of the error amplifying circuit  
AMP1, and a voltage drop by a wiring resistance from  
the constant-voltage circuit unit 2 to the load 10.

Further, the present invention is not  
limited to these embodiments, but various variations  
20 and modifications may be made without departing from  
the scope of the present invention.